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**Residential heating and cooling with Aquifer Thermal Energy Storage (ATES) on city scale** 

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1. Research goal	2. Methods
<ul> <li>Aquifer thermal energy storage (ATES) enables seasonal storage of thermal energy in groundwater.</li> </ul>	Simple and fast-to-compute 3D thermo-hydraulic numerical box models approximating the Freiburg subsurface conditions of three designated hydrogeological regions within the study area
This study quantifies the technical potential of shallow Low-Temperature (LT-ATES) in the city of Freiburg im Breisgau, Germany by means of spatially distributed power	<ul> <li>Simulation of 1-, 2- and 3-doublet ATES systems dependent on groundwater flow in</li> </ul>

- density [W m<sup>-2</sup>].
- Possible heating and cooling supply rates of ATES are calculated by comparing power densities with existing heating and cooling demands.



Fig. 1: Model area located in the city of Freiburg im Breisgau: Map overview and profle section A – A\* (modified from [1]).

## 3. Results and discussion



Thermal recoveries (Fig. 3) are consistently higher for ATES systems in the Breisgau Formation compared to systems in the Neuenburg Formation (Fig. 2). Accordingly, the highest ATES power densities (Fig. 4) are determined for 3-doublet

supply rates of residential

**Crystalline Basement** 

order to achieve highest thermal recoveries TR:

$$TR = \frac{E_{extr}}{E_{inj}} = \frac{\int_{extr \ start}^{extr \ end} \dot{V}_{extr} \cdot (T_{extr} - T_{amb}) \ dt}{\int_{inj \ start}^{inj \ end} \dot{V}_{inj} \cdot (T_{inj} - T_{amb}) \ dt}$$

The power density relates the ATES heating and cooling power to the required horizontal Earth surface, i.e. the thermally affected zone TAZ (Fig. 2).



## temperature [°C]

- Simulated ATES operation:
- Pumping rate =  $600 \text{ m}^3 \text{ d}^{-1}$
- Injection temperature of warm water = 18 °C
- Injection tempeature of cold water = 6 °C
- 4 months heating and 4 months cooling per year
- Two 2-months pasive storage periods
- Fig. 2: Exemplary box model of a 2-doublet ATES system in the Neuenburg Formation. The TAZ around the ± 0.5 K-isotherms after 30 years of operation is highlighted.
- Separate calculation of heating and cooling power densities PD:

$$PD_{heating} = \frac{\bar{P}_{heating} \cdot f_{ava}}{A_{TAZ} \cdot 0.5} \quad \text{with}$$
  
$$\bar{P}_{heating} = \dot{V}_{extr} \cdot \rho_f c_{p,f} \cdot \left[ (T_{inj,warm} - T_{amb}) \cdot TR + (T_{amb} - T_{inj,cold}) \right] \cdot \frac{COP}{COP - 1}$$

Fig. 3: Thermal recovery values for various ATES configurations in different groundwater flow regimes.



Fig. 4: ATES power densities for 2-doublet systems (Neuenburg Formation) and for 3-doublet systems (Breisgau Formation).



demands. The highest supply rates can be observed for suburban and commercial districts. Based on these supply rates, Fig. 6 shows possible greenhouse gas (GHG) emission savings calculated from a typical ATES heating emission factor and the current heating supply mix in Freiburg. 109 Emissions of current supply mix **GHG** emission savings: Emissions of ATES supply 70 ktCO<sub>2eq</sub> a<sup>-1</sup> GHG emission savings: 17 ktCO<sub>2eq</sub> a<sup>-1</sup> 9

$$PD_{cooling} = rac{\overline{P}_{cooling} \cdot f_{ava}}{A_{TAZ} \cdot 0.5}$$
 with

$$\bar{P}_{cooling} = \dot{V}_{extr} \cdot \rho_f c_{p,f} \cdot \left[ (T_{amb} - T_{inj,cold}) \cdot TR + (T_{inj,warm} - T_{amb}) \right]$$

Calculation of heating and cooling supply rates SR from power densities PD and energy demand *ED*:









Fig. 6: Possible greenhouse gas (GHG) emission savings from ATES heating compared to the current heating energy mix in the city of Freiburg. Calculated for two scenarios based on data from [5,6].





supply rate [%]

Fig. 5: ATES supply rates in the city of Freiburg for heating and cooling using the Breisgau Formation. The bar charts illustrate the share of the total residential buildings in each individual supply rate class.

4. Conclusion	References
<ul> <li>The technical potential of LT-ATES is quantified for the city of Freiburg by determining ATES power densities using numerical 3D heat transport models.</li> <li>Multi-doublet ATES designs reduce subsurface thermal energy storage loss.</li> <li>Thermal recoveries of up to 59 % can be obtained for ATES in the deeper aquifer with lower groundwater flow velocities.</li> <li>ATES power densities of up to 3.2 W m<sup>2</sup> are determined.</li> <li>Residential ATES heating supply rates of more than 60 % are determined for about 50 % of all buildings. 100 % ATES cooling supply is possible for 92 % of the buildings.</li> <li>GHG emission savings of up to 70,000 tCO<sub>2</sub>eq a<sup>-1</sup> resulting from ATES heating alone are estimated.</li> </ul>	<ol> <li>Wirsing, G., Luz, A. (2005): Hydrogeologischer Bau und Aquifereigenschaften der Lockergesteine im Oberrheingraben (Baden-Württemberg). Regierungspräsidium Freiburg, Abteilung 9 Landesamt für Geologie, 775 Rohstoffe und Bergbau (LGRB), Freiburg i. Br.</li> <li>Gizzi, M., Taddia, G., Abdin, E. C., Lo Russo, S. (2020): Thermally Affected Zone (TAZ) Assessment in Open-Loop Low-Enthalpy Groundwater Heat Pump Systems (GWHPs): Potential of Analytical Solutions. Geofluids; 2020:1–13.</li> <li>Lo Russo, S., Taddia, G., Verda, V. (2012): Development of the thermally affected zone (TAZ) around a groundwater heat pump (GWHP) system: A sensitivity analysis. Geothermics; 43:66–74.</li> <li>Piga, B., Casasso, A., Pace, F., Godio, A., Sethi, R. (2017): Thermal Impact Assessment of Groundwater Heat Pumps (GWHPs): Rigorous vs. Simplified Models. Energies; 10:1385.</li> <li>GEF Ingenieur AG, ifeu - Institut für Energie- und Umweltforschung gGmbH, badenova-Gruppe (2021): Masterplan Wärme Freiburg 2030.</li> <li>Stemmle, R., Blum, P., Schüppler, S., Fleuchaus, P., Limoges, M., Bayer, P., Menberg, K. (2021): Environmental impacts of aquifer thermal energy storage (ATES). Renewable and Sustainable Energy Reviews; 151:111560.</li> </ol>

